# PATENT ABSTRACTS OF JAPAN

(11)Publication number:

2001-078459

(43)Date of publication of application: 23.03.2001

(51)Int.Cl.

H02M 7/12 H02M 3/155

H02M 7/48

(21)Application number : 11-253110

(22)Date of filing:

07.09.1999

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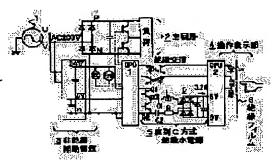
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# (54) SERIES C-SYSTEM INSULATION POWER SUPPLY

#### (57)Abstract:

PROBLEM TO BE SOLVED: To improve a capacitor insulation type power supply by connecting a non-insulated auxiliary power supply to an AC voltage source, further connecting in series a capacitor, a reactor and a diode rectifier to a high-frequency power supply provided in this auxiliary power supply, and moreover forming a small capacity insulation power supply.

SOLUTION: A non-insulated auxiliary power supply 3 is connected to a commercial 50 Hz or 60 Hz AC 200 V power supply 1, in addition to a main circuit 2 of several kW consisting of a diode-rectified DC power supply PN, power transistor and load or the like. A high-frequency power supplies Q1, Q2 is formed in the auxiliary power supply 3, capacitors C1, C2, reactor L and diode rectifier D are connected to these high frequency power supplies Q1, Q2 to form a small size serial C-system insulation power supply 5. As a result, a loss of zener diode can be suppressed by conducting the feedback control.



## LEGAL STATUS

[Date of request for examination]

14.03.2003

[Date of sending the examiner's decision of rejection]

26.05.2005

[Kind of final disposal of application other than the examiner's decision of rejection or application converted registration]

[Date of final disposal for application]

[Patent number]

[Date of registration]

[Number of appeal against examiner's decision of rejection]

[Date of requesting appeal against examiner's decision of rejection]

[Date of extinction of right]

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#### **CLAIMS**

#### [Claim(s)]

[Claim 1] The serial C method insulation form power source characterized by acquiring the insulating power source of small capacity further by connecting non-insulating auxiliary power to the source of alternating voltage apart from a main circuit, and connecting a capacitor, a reactor, and a diode rectifier to a serial to the RF generator prepared in this auxiliary power.

[Claim 2] The serial C method insulation form power source according to claim 1 characterized mainly by applying to the actuation display of an electric product or a device.

[Claim 3] The serial C method insulation form power source according to claim 1 characterized by setting to 10mA or less the current at the time of the ground of the electric product to which a power source is supplied, or a device.

[Claim 4] the time of setting the impedance in the RF of said capacitor and a reactor to 1-/omegaC and omegaL (omega: angular frequency), respectively — omegaL>1/omegaC — the serial C method insulation form power source according to claim 1 characterized by making it fill relation.

[Claim 5] The serial C method insulation form power source according to claim 1 characterized by replacing with said reactor and using resistance.

[Claim 6] The RF generator in said auxiliary power is a serial C method insulation form power source according to claim 1 characterized by being one inverter of a vertical one arm each.

[Claim 7] The RF generator in said auxiliary power is a serial C method insulation form power source according to claim 1 which considers as the inverter of vertical two arms each, and is characterized by inserting the capacitor of the same configuration, and the series circuit of a reactor in this.

[Claim 8] The serial C method insulation form power source according to claim 1 characterized by performing feedback control of output voltage.

[Translation done.]

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#### DETAILED DESCRIPTION

[Detailed Description of the Invention]

[0001]

[Field of the Invention] This invention is used for various electric products, and relates to a suitable insulating form power source, especially its amelioration.

[0002]

[Description of the Prior Art] The auxiliary power used for the drive of the actuation control power source used as the brains section, i.e., CPU, a display lamp, a cooling fan, and a relay etc. is un-insulating in many cases. The control unit as a part which people touch directly or indirectly and operate among the auxiliary power of this not insulating has the case where he wants to carry out insulating separation with a main circuit. Moreover, even if people do not touch, the case where he wants to supply a small power source is in a part to carry out the insulation for bearing the ground and an external noise. As such a power source, for example, an insulating power source is prepared independently conventionally, and there are some which communicate with non-insulating auxiliary power, a photo coupler, etc.

[0003]

[Problem(s) to be Solved by the Invention] However, generally an insulating power source has the problem of becoming expensive. On the other hand, the power source by "the DC-DC converter by capacitor insulation of the Heisei 6 Institute of Electrical Engineers of Japan semi-conductor power conversion study group, SPC-94-18, and 1994 announcements", i.e., a capacitor insulation method, is mentioned as a technique applicable to this invention. Therefore, the technical problem of this invention is shown in aiming at amelioration of a capacitor insulation method power source.

[0004]

[Means for Solving the Problem] In order to solve such a technical problem, in invention of claim 1, it is characterized by acquiring the insulating power source of small capacity further by connecting non-insulating auxiliary power to the source of alternating voltage apart from a main circuit, and connecting a capacitor, a reactor, and a diode rectifier to a serial to the RF generator prepared in this auxiliary power. Invention of above-mentioned claim 1 can set to 10mA or less the current at the time of the ground of the electric product to which it can apply to the actuation display of an electric product or a device (invention of claim 2), or a power source is mainly supplied, or a device (invention of claim 3).

[0005] the time of setting the impedance in the RF of said capacitor and a reactor to 1-/omegaC and omegaL (omega: angular frequency) in invention of above-mentioned claim 1, respectively — omegaL>1/omegaC — it can make it possible to fill relation (invention of claim 4), or it can replace with said reactor, and resistance can be used (claim 5 invention). Furthermore, in invention of above-mentioned claim 1, the RF generator in said auxiliary power can be one inverter of a vertical one arm each (invention of claim 6), or the RF generator in said auxiliary power can be used as the inverter of vertical two arms each, and the capacitor of the same configuration and the series circuit of a reactor can be inserted in this (invention of claim 7), or feedback control of output voltage can be performed (invention of claim 8).

[0006]

[Embodiment of the Invention] <u>Drawing 1</u> is the circuit diagram showing the gestalt of implementation of this invention. The several kW main circuit which consists of DC power supply PN and the power transistor with which 1 carried out commercial 50 or AC200V 60Hz commercial power source, and 2 carried out diode rectification of this, a load, etc., and 3 show non-insulating auxiliary power. Although the serial R method which connected resistance to the switching regulator, the power source, and the serial, the serial C method which connected the capacitor at the power source and the serial are considered variously at this auxiliary power 3, it considers as two outputs of 24V and 5V by the serial C method, and direct continuation of the terminals N and n is carried out here. CPU1 connected with 5V is formed as main objects for control of this equipment, and manages control of the power transistors Q1 and Q2 which constitute Relay RY, Fan FAN, and the small power source of high frequency.

[0007] 4 is an actuation display and is a part which displays the condition of equipment with a light emitting diode, or pushes the contact of a touch panel with a finger, performs switching operation, and inputs operator command, such as starting and a halt, into the body of equipment. For example, between a finger and a contact, although it insulates with about 0.1mm strong insulating film 6, when dielectric breakdown should occur in this, it may become the major accident which participates in a human life directly. A non-insulating method is permitted only to the particular application which the limited man operates, although there is usually 5kV or more of withstand voltage of a film and it is generous enough. For this reason, he forms another CPU2 in a control unit, and is trying to insulate in CPU1.

[0008] Here, the level of an insulation poses a problem. That is, when it is several A or less [ in which 1 equipment does not break ] as a ground current which flows when the actuation display 4 should carry out the ground, even if a ground current number A Flows, an earth leakage breaker operates without equipment breaking, and the insurance of equipment and the body can be secured.

- 2) When the body is several safe mA or less, suppress a ground current to several mA sufficiently lower than the 10mA of the risk level number of the bodies. It is almost safe even if an earth leakage breaker does not operate.
- 3) Hold down without the leakage current to the ground current below several microA. Important for a measuring instrument, others, and a particular application.

Although which case can be considered, it is appropriate to choose the 2nd above-mentioned term with the various electric products containing an electrical home appliance.

[0009] The small transistors Q1 and Q2 as a small power source of the high frequency shown in <u>drawing 1</u> are turned on and turned off by turns, and the high-frequency ac electrical potential difference of 12V of hundreds of kHz is generated from 24V direct current. Then, by C1, L, the diode rectifier, and C2 grade When the operating power source (<u>drawing 1</u> shows as a serial C method insulation smallness power source 5) of about 0.2mA, and 5V and 1W shall be obtained, the value of C1 and C2 which hold down the value of a ground current to several mA or less is about 0.02 micro F.

It turns out that it is set to C1+C2=0.04microFf=60HzE=200V ground current it=2pifCE=3.02mA, and conditions are fulfilled. [0610] In order to rectify the current from the above-mentioned RF smallness power source and to obtain about 0.2A and 5V E=12-6=6V (this assumes lengthening by six [ V ] from supply voltage, although outputted 5V.) The proper frequency f and an inductance L are set to f=270kHzL=50microhenry again. Capacity C as a serial value of the above C1 and C2 C= 1/(1 / C 1+1 / C2) = 0.01 micro F to the high frequency current ih is ih=E/(2pifL-1/2pifC) =0.232A (about 0.2A).

A next door and conditions are fulfilled.

[0011] Here, the reactor L inserted between the transistors Q1 and Q2 as a small power source of the high frequency within a power source 5 and diode rectifier D carries out important work. That is, the current ic in case this L does not exist is set to ic=2pifCE=0.102A, and is quite smaller than the above. And if supply voltage (12V) is higher than output voltage (5V) enough, in fact, only by C, smooth rectification cannot be performed, but smooth rectification can be performed only after there is L, and it will be said that sufficient current can be supplied. Moreover, when setting the impedance of C and L to 1-/omegaC and omegaL (omega: angular frequency), respectively, also experimentally, it is confirmed that it is good to make the ratio about into about 3:2.

[0012] That is, the synthetic impedance Z of C and L is Z=j (L-1/omegaC of omega).

It is because the big output current can be taken by C with more nearly same having come out and making Z small, and is made the lagging current as L> 1/omegaC of omega because it is also indispensable business for Q1 and Q2 to operate to stability by the RF. In addition, since it will not be stabilized if the above-mentioned ratio is brought close to 1:1 and it changes into a series resonance condition, the device of adding R then is needed. Moreover, if it does not care about loss; only R is usable instead of L. In addition, although it became clear that various capacitor insulation methods like SPC-94-18 are proposed as a result of investigation, it adds that there was nothing that uses L in order to perform smooth rectification and to supply sufficient current.

[0013] Although the small power source of the high frequency within the serial C method insulation smallness power source 5 was considered as the half bridge configuration of Q1 and Q2 in <u>drawing 1</u>, by considering as the full bridge configuration of Q1-Q4 like <u>drawing 2</u>, preparing L1 and L2 and considering as vertical symmetry structure, a noise can be decreased (negating a noise) and stability can be increased. Moreover, if Controller Reg performs feedback control through a photo coupler etc. so that output voltage may become fixed 5v, loss by zener diode can be suppressed and a power source with little loss can be offered.

[Effect of the Invention] According to this invention, as auxiliary power of the part from which insurance, such as an actuation display, poses a problem, since the serial C method insulation form power source was used, a cheap and practical insulating power source is realizable.

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#### **DESCRIPTION OF DRAWINGS**

[Brief Description of the Drawings]

[Drawing 1] It is the circuit diagram showing the gestalt of implementation of this invention.

[Drawing 2] It is the circuit diagram showing another example of the insulating smallness power source shown in drawing 1.

[Description of Notations]

1 [ -- An actuation display 5 / -- A serial C method insulation smallness power source, 6 / -- Insulating film. ] -- AC power supply, 2

- A main circuit, 3 - Non-insulating auxiliary power, 4

[Translation done.]

### (19)日本国特許庁 (JP)

# (12) 公開特許公報(A)

(11)特許出願公開番号 特開2001-78459 (P2001-78459A)

(43)公開日 平成13年3月23日(2001.3.23)

(51) Int.Cl. <sup>7</sup>	識別記号FI			テーマエード( <del>参考</del> )		
H02M	7/12		H 0 2 M	7/12	Y	5 H O O 6
	3/155			3/155	н	5 H O O 7
	7/48			7/48	Τ	5 H 7 3 0

#### 審査請求 未請求 請求項の数8 OL (全 4 頁)

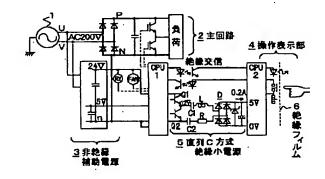
	<b>若</b> 登前 次	未請求 請求項の数8 UL (全 4 貝)		
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## (54) [発明の名称] 直列C方式絶縁形電源

#### (57)【要約】

【課題】 商用周波の地絡電流を、人体等に影響を及ぼさない数m A程度に抑制可能な電源を提供する。

【解決手段】 主回路2とは別に非絶縁の補助電源3内 に高周波電源Q1, Q2を形成し、これに直列にコンデンサC1, C2とリアクトルLおよびダイオード整流器 Dを接続してさらに小さな絶縁小電源5を形成することで、安価で実用的な絶縁電源を実現する。



#### 【特許請求の範囲】

【請求項1】 交流電圧源に主回路とは別に非絶縁の補 助電源を接続し、との補助電源内に設けられた高周波電 源に対してコンデンサとリアクトルとダイオード整流器 とを直列に接続することにより、さらに小容量の絶縁電 源を得ることを特徴とする直列C方式絶縁形電源。

【請求項2】 主として、電気製品または機器の操作表 示部に適用することを特徴とする請求項1に記載の直列 C方式絶縁形電源。

地絡時の電流を、10mA以下とすることを特徴とする 請求項1 に記載の直列C方式絶縁形電源。

【請求項4】 前記コンデンサ、リアクトルの高周波で のインピーダンスをそれぞれ1/ωC, ωL(ω:角周 波数)とするとき、

#### $\omega L > 1 / \omega C$

なる関係を満たすようにすることを特徴とする請求項1 に記載の直列C方式絶縁形電源。

【請求項5】 前記リアクトルに代えて抵抗を用いると とを特徴とする請求項1に記載の直列C方式絶縁形電 源。

【請求項6】 前記補助電源内の高周波電源は、上下各 1アームの1つのインバータであることを特徴とする請 求項1に記載の直列C方式絶縁形電源。

【請求項7】 前記補助電源内の高周波電源は上下各2 アームのインバータとし、これに同一構成のコンデン サ、リアクトルの直列回路を挿入することを特徴とする 請求項1に記載の直列C方式絶縁形電源。

【請求項8】 出力電圧のフィードバック制御を行なう ことを特徴とする請求項1に記載の直列C方式絶縁形電 30 源。

#### 【発明の詳細な説明】

#### [0001]

【発明の属する技術分野】この発明は、各種電気製品に 使用して好適な絶縁形電源、特に、その改良に関する。 [0002]

【従来の技術】頭脳部となる操作制御電源、すなわちC PU、表示ランプ、冷却ファン、リレーの駆動などに使 用される補助電源は、非絶縁となっている場合が多い。 この非絶縁の補助電源のうち、人が直接または間接に接 40 して操作する部分としての操作部は、主回路と絶縁分離 したい場合がある。また、人が接しなくても、地絡や外 部ノイズに耐えるための絶縁がしたい部分に小電源を供 給したい場合がある。とのような電源として、従来は例 えば絶縁電源を別に用意して、非絶縁の補助電源とフォ トカプラなどで交信するものがある。

## [0003]

【発明が解決しようとする課題】しかし、一般に絶縁電 源は髙価になるという問題がある。一方、平成6年電気 94発表の「コンデンサ絶縁によるDC-DCコンバー タ」、すなわちコンデンサ絶縁方式による電源が、この

発明に適用可能な技術として挙げられる。したがって、 との発明の課題はコンデンサ絶縁方式電源の改良を図る ととにある。

#### [0004]

【課題を解決するための手段】このような課題を解決す るため、請求項1の発明では、交流電圧源に主回路とは 別に非絶縁の補助電源を接続し、この補助電源内に設け 【請求項3】 電源を供給される電気製品または機器の 10 られた高周波電源に対してコンデンサとリアクトルとダ イオード整流器とを直列に接続することにより、さらに 小容量の絶縁電源を得ることを特徴とする。上記請求項 1の発明は、主として、電気製品または機器の操作表示 部に適用することができ(請求項2の発明)、または、 電源を供給される電気製品または機器の地絡時の電流 を、10mA以下とすることができる(請求項3の発 明)。

> 【0005】上記請求項1の発明においては、前記コン デンサ、リアクトルの高周波でのインピーダンスをそれ 20 ぞれ  $1/\omega C$ ,  $\omega L$  ( $\omega$ :角周波数)とするとき、  $\omega L > 1 / \omega C$

なる関係を満たすようにすることができ (請求項4の発 明)、または、前記リアクトルに代えて抵抗を用いると とができる(請求項5発明)。さらに、上記請求項1の 発明においては、前記補助電源内の高周波電源は、上下 各1アームの1つのインバータであることができ(請求 項6の発明)、または、前記補助電源内の髙周波電源は 上下各2アームのインバータとし、これに同一構成のコ ンデンサ、リアクトルの直列回路を挿入することができ (請求項7の発明)、もしくは、出力電圧のフィードバー ック制御を行なうことができる(請求項8の発明)。 [0006]

【発明の実施の形態】図1はこの発明の実施の形態を示 す回路図である。1は商用の50または60HzのAC 200 V電源、2はこれをダイオード整流した直流電源 PNとパワートランジスタ,負荷などからなる数kWの 主回路、3は非絶縁の補助電源を示す。この補助電源3 にはスイッチングレギュレータ、電源と直列に抵抗を接 続した直列R方式、電源と直列にコンデンサを接続した 直列C方式などいろいろ考えられるが、ここでは直列C 方式による24Vと5Vの2出力とし、端子Nとnを直 接接続している。5VにつながるCPU1はこの装置の 主な制御用として設けられ、リレーRY、ファンFA N、高周波の小電源を構成するパワートランジスタQ 1. Q2などの制御を司る。

【0007】4は操作表示部で、発光ダイオードで装置 の状態を表示したり、指でタッチパネルの接点を押して 開閉操作を行ない、装置本体に起動、停止などの操作指 令を入力する部分である。例えば指と接点との間は、約 学会半導体電力変換研究会,SPC-94-18,19 50 0.1mmの丈夫な絶縁フィルム6で絶縁されるが、万

一これに絶縁破壊が発生すると、人命に直接関与する重大事故になりかねない。フィルムの絶縁耐圧は通常5kV以上あり十分余裕はあるが、非絶縁方式は限られた人が操作する特殊用途にしか許可されない。このため、操作部には別のCPU2を設け、CPU1とは絶縁するようにしている。

【0008】 ここで、絶縁のレベルが問題となる。すなわち、操作表示部4が万一地絡したとき流れる地絡電流としては、

1) 装置が壊れない数A以下のとき 地絡電流が数A流れても、装置が壊れずに漏電遮断器が 作動して、装置と人体の安全が確保できる。

2) 人体が安全な数mA以下のとき

地絡電流を人体の危険レベル数十mAより十分低い数mAに抑える。漏電遮断器が作動しなくても、ほぼ安全である。

3)漏れ電流なしで、数μA以下の地絡電流に抑える。 計測器その他、特殊用途には重要。

などの場合が考えられるが、家庭電化製品を含む各種電気製品では、上記2)項を選ぶのが適当である。

【0009】そとで、図1に示す高周波の小電源としての小トランジスタQ1,Q2を交互にオン、オフして、24 V 直流から数百 k H z の12 V の高周波交流電圧を発生し、C1、 L、ダイオード整流器、C2 等により、約0.2 m A、5 V、1 W の操作電源(図1 では、直列 C 方式絶縁小電源5 として示す)を得るものとすると、地絡電流の値を数 m A 以下に抑えるC1,C2 の値は約0.02  $\mu$  F である。

 $C1 + C2 = 0.04 \mu F$ 

f = 60 Hz

E = 200V

地絡電流 i  $t = 2\pi f CE = 3$ . 02mAとなり、条件を満たすことが分かる。

[0010]上記高周波小電源からの電流を整流して約 0.2A,5Vを得るには、E=12-6=6V (これは、5V出力するのに電源電圧から6V分引かれることを想定している。)また、適正な周波数 f, インダクタンスLを、

f = 270 kHz

 $L = 50 \mu H$ 

とし、容量Cは上記C1, C2の直列値として、

 $C = 1 / (1/C1 + 1/C2) = 0.01 \mu F$ 

から、高周波電流ihは、

 $i h = E / (2 \pi f L - 1 / 2 \pi f C) = 0.232 A$ (\(\frac{2}{3}0.2A\)

となり、条件を満たしている。

【0011】ここで、電源5内の高周波の小電源としてのトランジスタQ1、Q2と、ダイオード整流器Dとの

【0012】つまり、CとLの合成インピーダンスZ tt

 $Z = i (\omega L - 1/\omega C)$ 

で、Zを小さくしたほうが同じCで大きな出力電流をとれるからであり、また、ωL>1/ωCとして遅れ電流にするのは、Q1,Q2が高周波で安定に動作するための必須用件でもあるからである。なお、上記比を1:1に近づけて直列共振状態にすると安定しないので、そのときはRを追加するなどの工夫が必要となる。また、損20 失を気にしなければ、Lの代りにRのみでも実用可能である。なお、SPC-94-18のようなコンデンサ絶縁方式は種々提案されていることが調査の結果明らかになったが、円滑な整流を行ない十分な電流を供給する目的でLを利用するものはなかったことを付言する。

【0013】図1では直列C方式絶縁小電源5内の高周波の小電源をQ1、Q2のハーフブリッジ構成としたが、図2のようにQ1~Q4のフルブリッジ構成とし、L1、L2を設けて上下対称構造とすることにより、ノイズを減少させ(ノイズを打ち消し合わせて)安定性を30 増大させることができる。また、出力電圧が5V一定となるように、フォトカブラなどを介して調節器Regによりフィードバック制御を行なえば、ツェナーダイオードによる損失を抑えることができ、損失の少ない電源を提供することができる。

[0014]

【発明の効果】との発明によれば、操作表示部などの安全が問題となる部分の補助電源として、直列C方式絶縁形電源を用いるようにしたので、安価で実用的な絶縁電源を実現できる。

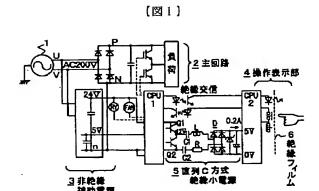
40 【図面の簡単な説明】

【図1】との発明の実施の形態を示す回路図である。 【図2】図1に示す絶縁小電源の別の例を示す回路図で

【図2】図1に示り起縁小竜像の例の例で示り凹凹図 ある。

【符号の説明】

1…交流電源、2…主回路、3…非絶縁補助電源、4… 操作表示部、5…直列C方式絶縁小電源、6…絶縁フィルム。



24V 01~04 D C1 L1 5V C2 L2 5V

[図2]

# フロントページの続き

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